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(54) **DEVICE AND METHOD FOR THE SURFACE PEENING OF A COMPONENT OF A GAS TURBINE**

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USPC 72/53; 29/90.7, 889.7
See application file for complete search history.

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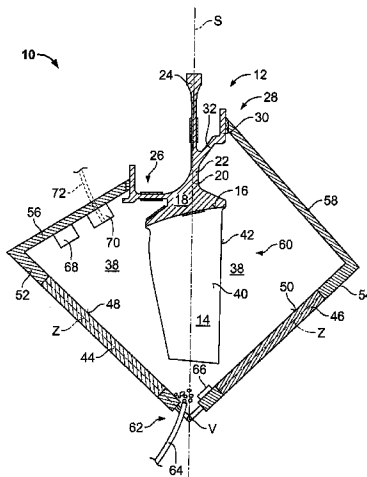
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(57) **ABSTRACT**

A device for surface-peening, especially for the ultrasound shot-peening of a component of a gas turbine, having at least one vibration means that comprises a surface that propels the peening material, and having a holding means with which a surface area of the component and the surface of the vibration means can be arranged with respect to each other is disclosed. In this context, the angular position of the surface of the at least one vibration means can be adjusted relative to the surface area of the component of the gas turbine. Moreover, a method is provided in which the angular position of the surface of the at least one vibration means can be adjusted relative to the surface area of the component.

12 Claims, 2 Drawing Sheets



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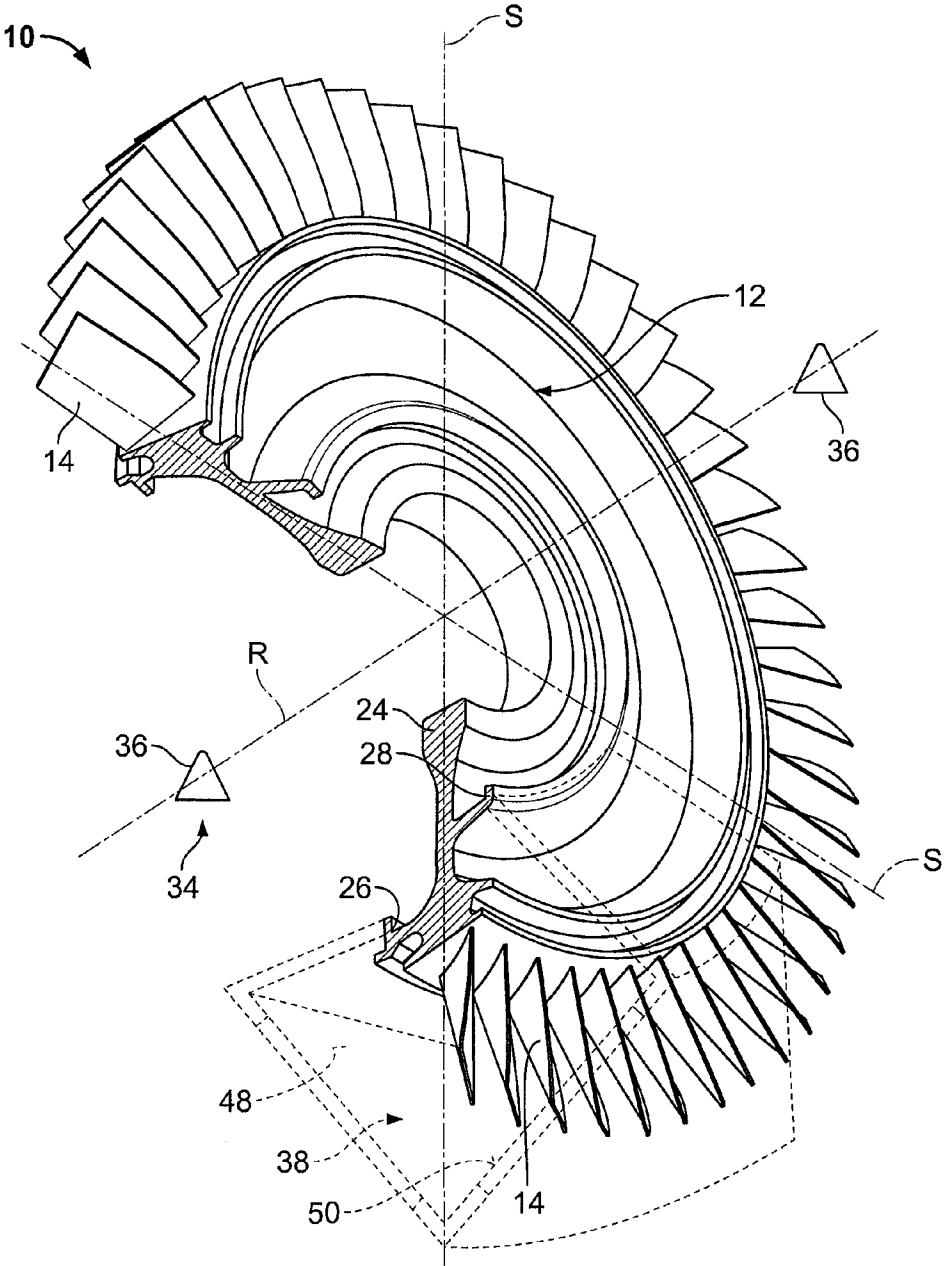


FIG. 1

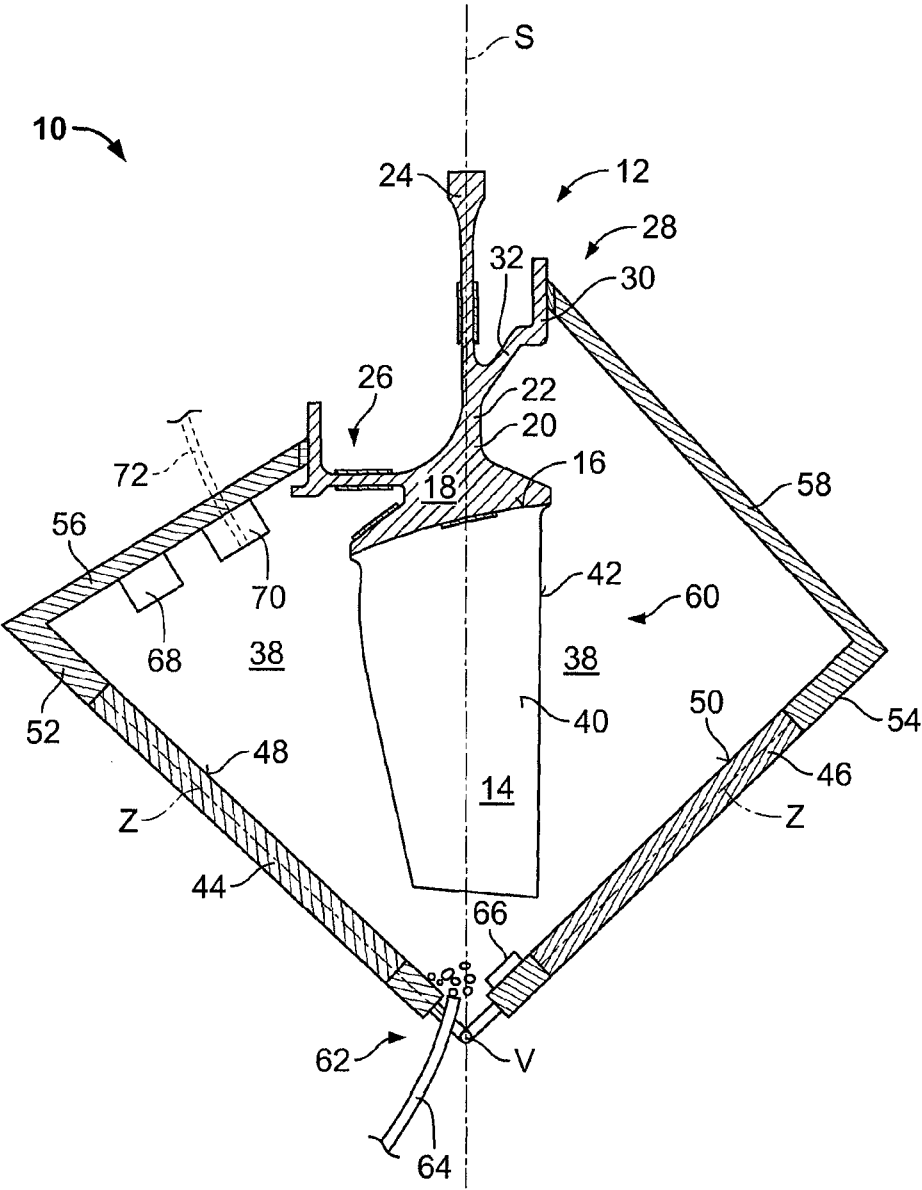


FIG. 2

**DEVICE AND METHOD FOR THE SURFACE
PEENING OF A COMPONENT OF A GAS
TURBINE**

Priority is claimed to German Patent Application DE 10 2006 058 679.4, filed Dec. 13, 2006 through international application PCT/DE2007/002195, filed Dec. 5, 2007, the entire disclosures of which are hereby incorporated by reference herein.

BACKGROUND OF THE INVENTION

The invention relates to a device for surface-peening, especially for the ultrasound shot-peening of a component of a gas turbine, having at least one vibration means that comprises a surface that propels the peening material, and having a holding means with which a surface area of the component and the surface of the vibration means can be arranged with respect to each other and to a method for surface-peening, especially for the ultrasound shot-peening of a component of a gas turbine in which a surface area of the component and at least one surface of the vibration means that propels the peening material are arranged with respect to each other and can be moved with respect to each other during the surface-peening.

Such a device and such a method are already known as prior art from European patent application EP 1 101 568 B1, whereby the rotor blades of a rotor configured as a blisk can be shot-peened for purposes of improving their fatigue strength. The device here comprises a holding means on which the rotor is held so as to be rotatable around its rotational axis. As the rotor turns, its blades pass through a peening chamber at the bottom of which there is a vibration means in the form of an ultrasound sonotrode having at least one vibrating surface that runs approximately horizontally. The peening chamber is delimited axially—that is to say, in the area of the wide sides of the rotor—as well as radially—in other words, in the area of the rotor blades of the blisk—by corresponding chamber walls. Since, depending on the position of each of the rotor blades, especially the walls of the peening chamber arranged radially with respect to the rotor are not capable of holding all of the balls inside the central peening chamber, two additional chambers are arranged upstream or downstream from the central peening chamber in the radial direction of the rotor. Balls that overflow from the central peening chamber fitted with the sonotrode are collected inside these additional chambers and returned via appropriate channels.

In this prior-art device and in the appertaining method, however, it can be considered as disadvantageous that it is very difficult to attain a uniform hardening of the surface areas of the rotor blades that are to be peened. This is also due to the fact that the rotor blades have a twist relative to their center axis or relative to the perpendicular to the rotational axis of the rotor.

SUMMARY OF THE INVENTION

Consequently, the objective of the present invention is to create a device as well as a method of the above-mentioned type by means of which various surface areas of the component can be hardened more systematically and more uniformly.

In order to allow various surface areas of components of the gas turbine to be hardened more systematically and more uniformly by surface-peening, it is provided according to the invention that the angular position of the surface of the at least one vibration means can be adjusted relative to the surface

area of the component of the gas turbine. For this purpose, with the method, it is provided according to the invention that the angular position of the surface of the vibration means can be adjusted relative to the surface area of the component before and/or during the surface-peening.

In other words, it is thus provided according to the invention that a device as well as a method for surface-peening are created with which the angular positions of the surface of the at least one vibration means and of the surface area of the component can be adjusted relative to each other in such a way that the specific surface area that is to be worked can be optimally peened with peening material. Since, for example, the twist of each rotor blade around its center axis or its perpendicular to the rotational axis of the rotor causes the vector of the surface normal to change markedly over the geometry of the blade, the fact that the surface of the vibration means can be adjusted now makes it possible to correspondingly adjust its normal vector. In other words, the surface of the vibration means, for instance, can now be adjusted in such a way that its normal vector—directly or at the desired angle—faces the surface area of the component that is to be worked. Since the angle at which the peening material is propelled from the surface of the vibration means against the surface area of the component that is to be worked has a decisive influence on the extent of the hardening, the latter can be systematically and uniformly adjusted by appropriately adjusting the angular position of the surface of the vibration means.

As a result, it can be seen that a systematic and uniform hardening of the surface of the component that is to be worked can be achieved in that the relative positions of the surface of the sonotrode and of the surface area that is to be worked are appropriately varied. In this context, it is conceivable to configure the surface of the vibration means so that it can be adjusted relative to the surface area that is to be worked as well as vice versa, namely, the surface area of the component can be adjusted—for example, using the holding means—relative to the surface of the vibration means.

Since the component of the gas turbine itself is secured by the holding means, the surface quality or the hardening of the surface area of the component to be worked can be reproduced very accurately. In other words, it can be ensured that the peening intensity of the surface-peening remains extremely homogenous within very narrow limits over the entire peening area.

The advantages of the device according to the invention cited below are also to be considered as advantages of the method according to the invention.

In another embodiment of the invention, it has also proven to be advantageous if the angular position of the surface of the at least one vibration means can be adjusted relative to the surface area during the surface-peening of the surface area of the component. As a result, various surface areas of the component can be worked individually by means of a surface-peening that is harmonized with said areas. Since, in each case, the angular position of the surface of the vibration means can be adjusted relative to the surface area that is to be worked, the peening intensity and the striking angle of the peening material can be harmonized with the surface area of the component that is to be worked. Here, for example, the rotor blades can be peened in a continuous or multiple-step process in that the rotor is turned at a certain speed. Consequently, the angular position of the surface of the vibration means changes as it adapts to the speed.

In another advantageous embodiment of the invention, two vibration means are provided which each have surfaces that are at an angle relative to each other. This makes it easy to

work a component on both sides simultaneously, so that even complex three-dimensional component geometries can be peened in an optimal manner. The simultaneous surface-peening on both sides entails the major advantage that, in particular, thin areas of the component do not become warped.

In this context, it has also proven to be advantageous for the appertaining surfaces of the two vibration means to be arranged so as to be essentially in a V-shape with respect to each other. The angular positions of these two surfaces can be adapted to each other very easily so that, especially in the case of peening on both sides, the surface areas that are directly across from each other can be peened simultaneously. A mirror-symmetrical arrangement provides that the appertaining surfaces of the two vibration means intersect each other at least approximately in a center axis or in a perpendicular of the component.

In another embodiment of the invention, the at least one adjustable surface of each vibration means can be adjusted around one or two adjustment axes. These two axes run preferably perpendicular to each other, so that a tilt angle and a rotational angle can easily be set. In other words, a surface of a vibration means that has two adjustment axes is thus especially characterized in that it can be adjusted two-dimensionally. Consequently, of course, the normal vector of the surface can also be adjusted two-dimensionally.

The device according to the invention has proven to be advantageous especially in order to peen a rotor, particularly a blisk, that is held so that it can rotate around its rotational axis. Especially the rotor blades can thus be easily brought into the peening area of the vibration means by turning the rotor, whereby the adjustable surface ensures that all of the surface areas that are to be worked are impinged with the desired peening intensity.

In order to be able to create a particularly simple device that yields an easily reproducible peening result, in another embodiment of the invention, it has proven to be advantageous to associate a peening chamber with the at least one vibration means, whereby the surface area of the component that is to be worked can be positioned in said peening chamber. It is obvious that the peening chamber has to be dimensioned large enough so that the surface of the vibration means can be set in all of the desired angular positions.

In another embodiment of the invention, the peening chamber can be easily adapted to the specific component that is to be worked in that its chamber walls are designed so as to be flexible, at least in certain areas. Such a flexible jacket makes it possible, for example, to surround the entire component, thus preventing the loss of peening material. Furthermore, such flexible chamber walls ensure that they can easily fit closely against the sonotrode and against the component holder, so that here as well, there is no need to fear any loss of peening material.

It has also proven to be advantageous for the angular position of the peening chamber walls themselves to be adjustable. As a result, on the one hand, the rebounding of the peening material from the chamber walls can be influenced and, on the other hand, the chamber walls can easily be moved close to the component in question in order to create a reliable seal to prevent peening material from escaping. It goes without saying that this makes it easy to use components having different geometries and sizes.

In another advantageous embodiment of the invention, a distribution means is provided with which the peening material can be distributed over the surface of the vibration means. Owing to the slanted arrangement of the surface, it is prevented in a simple manner that peening material accumulates

excessively at a low point of the surface. Instead, the distribution means can achieve a uniform distribution of the peening material, resulting in a uniform peening intensity over the entire surface and a uniform hardening of the surface area of the component.

It is possible to create a very simple distribution means if it comprises a vibrating surface which is configured, for example, as a sonotrode, a so-called flapper, a piezo shaker or a vibrating plate or membrane. As an alternative to this, the distribution means can also be operated with a compressed medium, especially with pressurized air, which can easily be adjusted in such a way that the peening material is uniformly distributed, also on the top places of the surface of the vibration means.

In another embodiment of the invention, for example, a first means for determining the quantity of peening material is provided inside the peening chamber. This means can perform, for instance, a sound analysis inside the peening chamber by means of which the quantity of peening material can be determined. This makes use of the underlying notion that the sound made by the peening material changes as a function of its quantity.

Moreover, in another embodiment of the invention, a means for refilling the peening material can be provided so as to keep the quantity of peening material constant inside the peening chamber. In particular, a uniform quantity of peening material ensures that the peening results are easily reproducible and constant.

Moreover, it has proven to be advantageous if the means for refilling the peening material can be controlled as a function of the quantity of peening material determined by the first means. In this manner, it is easy to perform monitoring, so that the same quantity of peening material is always present, for example, inside the peening chamber.

BRIEF DESCRIPTION OF THE DRAWING

Additional advantages, features and details of the invention can be gleaned from the description below of a preferred embodiment as well as on the basis of the drawings, without being limited thereto. The drawings show:

FIG. 1—a schematic perspective view of a rotor of a gas turbine—in the form of a blisk—depicted as a cutaway section that is held by means of a merely schematically indicated holding means so as to be rotatable around its rotational axis, whereby, on the bottom of the blisk in the area of the rotor blades, a schematically indicated peening chamber can be seen that comprises two surfaces—arranged in a V-shape with respect to each other—of associated vibration means with which peening material, for example, in the form of balls, can be propelled in the direction of the rotor blades; and in

FIG. 2—a schematic sectional view through the blisk according to FIG. 1, whereby, in the area of the rotor blades, the device for surface-peening is depicted that here comprises two surfaces—arranged in a V-shape with respect to each other—of each of the vibration means, whereby the angular positions of these two surfaces can be adjusted relative to the blisk.

DETAILED DESCRIPTION

FIG. 1 schematically shows a schematic and sectional perspective view of a rotatable rotor on a gas turbine in the form of a blisk 10. The basic individual areas of the blisk 10 can be seen in greater detail in conjunction with FIG. 2, which shows a schematic sectional view of said blisk 10. In particular, especially a blisk disk 12 can be clearly seen on whose outer

circumference numerous rotor blades **14** are arranged. A platform **16**—shown in the form of a line in FIG. 2—can be seen on the outer circumference of the blisk disk **12** and this platform **16** is followed radially towards the inside, or upwards in the drawing, by a sub-platform area **18**. This sub-platform area **18** makes a transition radially inwards into a disk neck **20** that connects the sub-platform area **18** to a disk element **22**. The radial inner end of the disk element **22** is formed by a hub **24** that constitutes a counterweight to the rotor blades **14**. A first wing **26**, whose cross section is essentially angular, projects from the sub-platform area **18** or from the disk neck **20** on one side of the blisk disk **12**. In a center area of the disk element **22**—as seen in the radial direction—another wing **28** projects from the other side of the blisk disk **12**, said wing comprising an angular area **30** as well as a web **32** that connects this area to the disk element **22**, said web projecting at an angle of 45° relative to the disk element **22**. All in all, the blisk **10** is configured to be rotatable around a rotational axis R or to be rotation-symmetrical.

As far as a device for the surface-peening of rotor blades **14** is concerned, FIG. 1 shows a holding means **34** symbolically indicated by two bearing blocks **36**, by means of which the blisk is held or mounted so as to be rotatable around its rotational axis R.

In addition to the holding means **34**, the shot-peening device here comprises a peening chamber **38** that can be seen in greater detail, especially when viewed in conjunction with FIG. 2. Here, the peening chamber **38** serves to shot-peen the surface areas **40**, **42** on the opposite sides of each of the rotor blades **14**. In FIG. 1, the peening chamber **38** is only indicated by broken lines and shown in a cutaway view along a perpendicular S on the rotational axis R of the blisk **10** or parallel to the sectional surface through the blisk **10**.

In FIG. 2, it can be seen that the peening chamber **38** comprises two vibration means **44**, **46**—indicated merely schematically—that are configured here as ultrasound sonotrodes. Each of the vibration means **44**, **46** has a surface **48**, **50** that faces the component to be peened or the appertaining rotor blade **14**, said surfaces **48**, **50** being configured flat in the present embodiment. In particular, it can be seen in FIG. 2 that the surfaces **48**, **50** of the two vibration means **44**, **46** are arranged essentially V-shaped with respect to each other, at an angle here of about 110° to 120°. The two vibration means **44**, **46** are accommodated inside appertaining chamber walls **52**, **54** of the peening chamber **38**. The chamber walls **52**, **54** that accommodate the vibration means **44**, **46** are followed at an angle by corresponding additional chamber walls **56**, **58** that close off the peening chamber **38** towards the top. Furthermore, on both faces **60**, chamber walls (not shown here) are provided that at least largely close off the peening chamber **38** in the radial direction of the blisk **10**.

It can be seen in FIG. 2 that the angular positions of the two surfaces **48**, **50** can be adjusted with respect to each other or to the component (rotor blades **14**) that are to be worked. Here, the adjustment axis V runs perpendicular to the plane of the page. Besides, each of the two surfaces **50** can be adjusted around another adjustment axis Z that is only schematically indicated in FIG. 2. In each case, the second adjustment axes Z each run in the plane of the surfaces **48**, **50** and perpendicular to the first adjustment axis V. In other words, each of the two surfaces **48**, **50** here are adjusted at least around the adjustment axis V and optionally—if present—around the additional adjustment axis Z. Consequently, either only a given tilt angle around the axis V or else additionally a rotation angle around the appertaining axis Z can be set in the present case. It goes without saying that, as a result, a normal vector or a perpendicular to the appertaining surface **48**, **50**

can be adjusted either unidimensionally or two-dimensionally. Therefore, it is achieved that different partial areas of the two opposite surface areas **48**, **50** of the appertaining rotor blades **14** can each be optimally hardened by means of the shot-peening. Since the rotor blades **14** each have a twist which, at different partial areas of their surface areas **40**, **42**, causes the vector of the surface normals to change markedly over the blade geometry, said change can be compensated for by appropriately adjusting the angle of the two surfaces **48**, **50** of the two vibration means **44**, **46**. Depending on the angular position of the two surfaces **48**, **50**, the striking angle of the peening material can be adjusted to the partial surface areas **40**, **42** to be peened, thus achieving optimal or individual hardening. The angular position of the surfaces **48**, **50** can be adjusted during the surface-peening of the rotor blade **14** in question, so that each rotor blade **14** can be surface-peened in a single work step. If the blisk **10** is rotated stepwise or continuously around its rotational axis R inside the holding means, then an adjustment can likewise be carried out by via the surfaces **48**, **50**.

As an alternative, of course, in an especially simple embodiment, it would naturally also be conceivable to configure the surfaces **48**, **50** so that they can only be adjusted in advance, whereby then the entire work process is carried out with the surfaces **48**, **50** that have been adjusted in this manner. This would be conceivable, for example, if the component to be worked has a relatively simple geometry. It is clear that the chamber walls **52**, **54**, **56**, **58** have to be appropriately configured so that the surfaces **48**, **50** of the two vibration means **44**, **46** can be adjusted. Here, it would be conceivable, for instance, to employ flexible chamber walls **52**, **54**, **56**, **58** that, in a simple manner, can even surround the entire component. This would create a flexible jacket that surrounds the entire component and fits closely against the side surfaces of the vibration means **44**, **46** and, if applicable, also against component holders (not shown here). In an embodiment not shown here, especially the chamber walls **56**, **58** that are located opposite from the surfaces **48**, **50** can likewise be configured so as to be adjustable in order to allow an appropriate adaptation to the slanted positioning of the vibration means **44**, **46**. In addition, adjustable chamber walls **56**, **58** can be employed to influence the deflection angle at which the peening material rebounds from the walls.

As a result of the V-arrangement of the two surfaces **48**, **50**, it is possible, in particular, to simultaneously peen opposite surface areas **40**, **42** of the appertaining rotor blades **14**. As a result, warping is prevented, especially in the case of components having fairly thin walls. Moreover, the adjustment of the angular positions of the surfaces **48**, **50** makes it possible to achieve a homogenous peening intensity over the entire peening area within narrow limits. In the present embodiment, the surfaces **48**, **50** are arranged at an identical angle relative to the perpendicular S, which constitutes a center axis through the appertaining rotor blade **14**. By the same token, of course, it would likewise be conceivable to set both surfaces **48**, **50** at different angles by means of the adjustment axes V and Z.

The two surfaces **48**, **50** can theoretically be set at an angle ranging from 0° to 90°, especially from 0° to 80°, relative to the perpendicular S or to the center axis of the appertaining rotor blades **14**. An angle of the two surfaces **48**, **50** with respect to the perpendicular S that is likewise well-suited is between about 30° and 60°, especially between 40° and 50°.

At the lowest point of the two surfaces **48**, **50**, a distribution means **62** is provided with which the peening material—primarily the balls—can be uniformly distributed over the two surfaces **48**, **50**. This likewise homogenizes the peening

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intensity. In the present embodiment, the distribution means **62** comprises a hose **64** through which pressurized air or compressed air can be fed in at the lowest point in the peening chamber **38**, so that peening material that is accumulating there can be moved upwards and uniformly distributed over the surfaces **48, 50**. As an alternative to the hose **64**, a vibrating surface **66** can also be provided, which is likewise schematically indicated in FIG. 2. In this context, the vibrating surface **66** can be operated by a sonotrode, a flapper, a piezo shaker or a vibrating plate or membrane. The result is that the peening material is uniformly distributed over the surfaces **48, 50**.

Moreover, a first means **68** with which the quantity of peening material can be ascertained is provided inside the peening chamber **38**. This can be done, for instance, on the basis of a sound analysis in which the sound in the peening chamber **38** is measured as a function of the quantity of peening material. When the value falls below a given threshold limit, additional peening material can be refilled with a second means **70**, as indicated by the hose **72** drawn with a broken line. The result is that a constant quantity of peening material is always present inside the peening chamber **38**, so that the peening results obtained are reproducible.

Therefore, for purposes of the surface-peening, the surface areas **40, 42** of the component **14** and the surfaces **48, 50** of the vibration means **44, 46** can be arranged relative to other by means of the holding means **32** and can be moved relative to each other by rotating the blisk **10** around its rotational axis R during the surface-peening. The angular position of the surface **48, 50** of the at least one vibration means **44, 46** relative to surface area **40, 42** of the component **14** can be adjusted either only in advance and/or during the surface-peening of the surface area **40, 42** of the component **14** so that the surface areas **40, 42** can be hardened systematically and uniformly.

The invention claimed is:

1. A device for surface-peening, especially for the ultrasound shot-peening of a component of a gas turbine, the component being a rotor having a hub and blades extending radially from the hub, the device comprising:

a peening chamber including a first vibrator having a first surface and a second vibrator having a second surface, the first and second surfaces forming a V-shape and

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being adjustable with respect to each other, the peening chamber including a first wall connected to the first vibrator and a second wall connected to the second vibrator, the first and second walls defining an opening therebetween for accepting the blades of the rotor and contacting the rotor so that the blades are within the peening chamber while the hub remains outside peening chamber; and

a holder capable of holding the rotor so that the blades can rotate with respect to the peening chamber.

2. The device as recited in claim **1**, wherein the rotor is a blisk.

3. The device according to claim **1**, further comprising a distributor with which the peening material can be distributed over the surface of the first and second vibrators.

4. The device according to claim **3**, wherein the distributor is arranged below a lowest point of the surface of the first and second vibrators.

5. The device according to claim **3**, wherein the distributor comprises a surface that propels the peening material, or else the distributor can be operated with a compressed medium with which the peening material can be uniformly distributed over the surface of the first and second vibrators.

6. The device according to claim **5**, wherein the compressed medium is pressurized air.

7. The device according to claim **1**, further comprising a first means for determining the quantity of peening material.

8. The device according to claim **1**, further comprising a second means for refilling peening material.

9. The device according to claim **8**, wherein the second means can be controlled as a function of the quantity of peening material determined by a first means for determining the quantity of the peening material.

10. The device according to claim **1**, wherein the first and second vibrators are adjustable about an axis perpendicular to a center axis of the turbine blade then being peened to adjust an angle between the first and second surfaces.

11. The device as recited in claim **1** wherein the first and second walls are flexible.

12. The device as recited in claim **10** wherein the angle is adjustable between 60 and 120 degrees.

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